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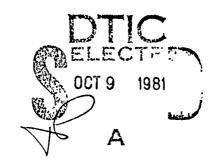
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MEMORANDUM REPORT ARBRL-MR-03125

COMBINATORIAL GEOMETRY COMPUTER MODELS OF SITTING AND STANDING CREW PERSONNEL

Loren R. Kruse Chit N. Lee

August 1981





US ARMY ARMAMENT RESEARCH AND DEVELOPMENT COMMAND BALLISTIC RESEARCH LABORATORY ABERDEEN PROVING GROUND, MARYLAND

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UNCLASSIFIED SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered) page Realings The Before Completing Form REPORT DOCUMENTATION PAGE 1. REPORT NUMBER 2. GOVT ACCESSION NO. 3. RECIPIENT'S CATALOG NUMBER MEMORANDUM REPORT ARBRL-MR-93125 -B060 1851 COMBINATORIAL GEOMETRY COMPUTER MODELS OF SITTING AND STANDING CREW PERSONNEL FINAL AU THOR(e) 8. CONTRACT OR GRANT NUMBER(a) Loren R. Kruse Chit N./ Lee 9. PERFORMING ORGANIZATION NAME AND ADDRESS 10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS USA Ballistic Research Laboratory 1L162618AH8Ø^r ATTN: DRDAR-BLV Aberdeen Proving Ground, MD 21005 11. CONTROLLING OFFICE NAME AND ADDRESS AUG**USU-1**981 US Army Armament Research & Development Comman US Army Ballistic Research Laboratory (DRDAR-BL) 13. NUMBER OF PAGE Aberdeen Proving Ground, MD 21005 4. MONITORING AGENCY NAME & ADDRESS(!! different from Controlling Office) 15. SECURITY CLASS. (of this UNCLASSIFIED 15a. DECLASSIFICATION/DOWNGRADING SCHEDULE 16. DISTRIBUTION STATEMEN I (of this Report) Distribution limited to US Government agencies only; Test and Evaluation: Aug 1981. Other requests for this document must be referred to Director, US Army Ballistic Research Laboratory, ATTN: DRDAR-TSB, Aberdeen Proving Ground, MD 21005. 17. DISTRIBUTION STATEMENT (of the ebetract entered in Block 20, if different from Report) 18. SUPPLEMENTARY NOTES 19. KEY WORDS (Continue on reverse side if necessary and identify by block number) GIFT Computer Code Target Description Personnel Description Crew Personnel Personnel Model Human Density COM-GEOM Description 28 ABSTRACT (Courtisus on reverse sich if necessary and identity by block number) Revised computer descriptions (models) of sitting and standing crew personnel have been generated using the Combinatorial Geometry (COM-GEOM) technique. These personnel models have been validated and have limited capability to be moved into various positions dependent on analytical requirements. The models generally correspond to the anthropometric data from the 50-60 percentile, grouping of US Army males. Appendix A discusses the calculation of an average human density based on the densities of bony and soft tissue.

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I. INTRODUCTION

New computer models of sitting and standing crew personnel have recently been constructed and are currently available for use in modifying and developing descriptive computer models of a variety of military systems considered for vulnerability analysis. The background for the generation of the computer models for the sitting and standing crew personnel grew out of training exercises involving the learning of the Combinatorial Geometry (COM-GEOM) technique of modeling militaring target systems.

Initially, approximately three years ago, the human head was selected as a subject for such a training exercise. The COM-GEOM model of the human head was subsequently completed and has remained, unuseful in its present state, until more recently, when the decision was made to complete the remainder of the crewman model. This decision evolved during the past year when the need appreciated for models of crew personnel that were more consistent with the level of detail in the COM-GEOM military target models currently being developed.

The new crew personnel models presented in this report are more anatomically detailed than the previously used models. This represents an improvement since the new models are more realistic and technically correct. However, this does not mean that the new models should be used for detailed studies involving human wound ballistics; further improvements in model detail could make such studies possible.

The sitting and standing crew personnel models were developed in two configurations, helmeted and unhelmeted, available in both inch and millimetre dimensional units. (The helmet is the only protective gear incorporated into the models.) Additionally, these models were developed with a feature which will allow them to be moved into various realistic positions; this will be discussed in a following section.

II. COMBINATORIAL GEOMETRY (COM-GEOM) MODELING TECHNIQUE

The generation of the computer models of the sitting and standing crew personnel utilize the COM-GEOM techniques of generating three dimensional models of objects. This technique provides compatible input data required to implement the Geometric Information for Targets (GIFT) computer code. Detailed discussion of the GIFT computer code and its many options are beyond the scope of this report; however, accounts of the COM-GEOM technique and its relationship to the GIFT code can be found in BRL Report No. 1802¹ and ARBRL Report No. 02189².

Lawrence W. Bain, Jr., and Mathew J. Reisinger, "The GIFT Code User Manual; Vol. I, Introduction and Input Requirements," USA Ballistic Research Laboratory Technical Report No. 1802, July 1975, DA#B006037L.

²Gary G. Kuehl, Lawrence W. Bain, Jr., and Mathew J. Reisinger, "The GIFT Code User Manual; Vol. II, The Output Options," USA Ballistic Research Laboratory Report No. 02189, Sept 1979, AD#A078364.

Only a brief familiarization with the COM-GEOM technique and terminology will be presented here.

The COM-GEOM technique provides up to twenty-three different types of basic geometric solids which may be assembled in combinations, as building blocks, to represent or "describe" a three dimensional (3-D) object. The geometric solids are combined in a prescribed manner, using selective set theory operations to generate the regions defining external and internal details of the 3-D object, such as shape, size, and location of various parts or components. The COM-GEOM computer model (description) contains three separate tables containing:

- Parametric data relating to the generation of the geometric solids comprising the model,
- Region data formed by the specific combination of the geometric solids, and
- Region identification data in which the regions are described verbally and given a specific numeric item descriptor.

The geometric solids available for use (and recognizable to the GIFT code) are listed in Table I. Parameters for each type of geometric solid listed must be tabulated in the manner prescribed in Reference 1. These parameters include characteristics which define the solid's physical size and exact location and orientation within a specified coordinate system.

There are no restrictions on the selection of geometric solids used in the modeling of an object. Ideally, a minimum number are used which would be sufficient to represent the level of detail desired for a specific model. Tables B-I and C-I list the geometric solids and their parameters used for the models of sitting and standing crew personnel respectively.

In forming the various components comprising a complex 3-D object, individual geometric solids are combined to form regions. A region is the volumetric space occupied by single or multiple solids. Solids are combined according to the following three set theory operations:

- Intersection (designated by a plus sign, +),
- Union (designated by an OR), and

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Subtraction (designated by a minus sign, -).

The Intersection (+) of two or more geometric solids defines the volumetric space common to the solids. The Union (OR) of two or more geometric solids defines the volumetric space within all the solids involved. The Subtraction (-) of two or more geometric solids defines

Table I. List of Geometric Solids Utilized in COM-GEOM Descriptions

Symbol for Solid Type	Solid Description
RPP	Rectangular Parallelepiped
BOX	Box
SPH	Sphere
RCC	Right Circular Cylinder
REC	Right Elliptical Cylinder
TRC	Truncated Right Angle Cone
ELL	Ellipsoids of Revolution
ELL1	(Input data differs slightly in ELL1)
ELLG	General Ellipsoid
RAW	Right Angle Wedge
ARB4	Arbitrary Convex Polyhedron of Four Sides
ARB5	Arbitrary Convex Polyhedron of Five Sides
ARB6	Arbitrary Convex Polyhedron of Six Sides
ARB7	Arbitrary Convex Polyhedron of Seven Sides
ARB8	Arbitrary Convex Polyhedron of Eight Sides
ARBN	Arbitrary Convex Polyhedron of N Sides
TEC	Truncated Elliptical Cones
TEC1	(Input data differs slightly in TEC1)
TGC	Truncated General Cone
HAF	Universe Dividing Plane
AQS	Arbitrary Quadratic Surface
TOR	Torus
ARS	Triangular Surfaced Polyhedron

the volumetric space contained in the first solid minus the volumes of the other intersecting solids. A two-dimensional analogical illustration displaying the effects of these three operations on three interacting solids is shown in Figure 1. Theoretically, any number of geometric solids may be used to define a region. In practice, regions are usually defined as representing some relatable component or part of a complex object. Each unique region with the combination of geometric solids defining it, are listed in the region data table. Tables B-II and C-II list the regions used in the sitting and standing man, respectively.

Each region of the model is assigned additional identification in the form of coded identification numbers and descriptive comments. The first of the coded identification numbers, termed an Item number, indicates the type or classification of the component the region represents. In most computer models of weapon systems regions are usually grouped according to the functions the involved components perform. Examples of such conventional groupings would be the missiles and cannisters and electrical and electronic components of a missile system. These groupings are usually designated by a three digit series number with the same first digit for the entire group. Another coded number assigned to a region indicates whether the region represents a volume of air; if greater than zero, it is either internal air somewhere within a target system or external air. Here again, certain conventions are used to distinguish the various air codes. Since the computer models of crew personnel are not as complex as models of weapon or other target systems, the coded identification numbers are not utilized to their fullest extent. The region identification table also allows up to 40 alphanumeric characters which will be used for a verbal description of the region. Associated with this description are two additional coded numbers indicative of the type of material the region is basically made of and a percentage number associated with an equivalent line-of-sight (LOS) thickness of the region. These latter numbers are required input for a typical vulnerability analysis. Tables B-III and C-III list in numerical order the regions and their appropriate identification. Tables B-IV and C-IV list the regions and their identification numbers ordered by Item numbers.

Tables B-I, B-II, and B-III and C-I, C-II, and C-III form the complete COM-GEOM computer models of the sitting and standing crew personnel, respectively.

III. COM-GEOM MODELS OF CREW PERSONNEL

The computer models of the sitting and standing crew personnel represent combat soldiers approximately 1.75 metres (5 feet 9 inches) in height with body measurements scaled from men of average mesomorphic proportions. Initial measurements used for these models were generated independently, unbiased by those of the previous computer models of sitting and standing man. It was noted that some measurements on both the previous and new models were very similar in size. The initial

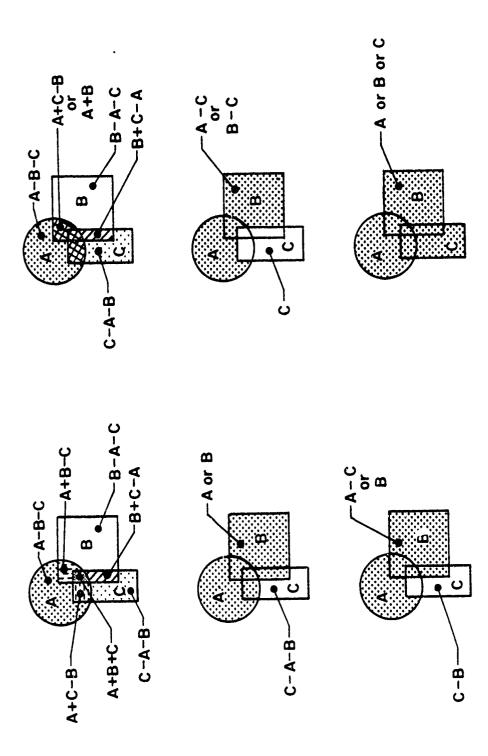


Figure 1. Regions (·) Formed When Using Intersection (+), Union (OR), and Subtraction (-) Operations on Three Interacting Solids

measurements for the new models were taken from male Bullistic Research Laboratory personnel and adjusted on the basis on what was considered to be "average." Later adjustments were made based on anthropometric data for US Army soldiers. Figures 2 and 3 indicate which basic measurements were used in the adjustment process. The comparison of the measurements from actua! US Army soldiers and the computer models is shown in Table II. The measy ement data from the data from the soldiers represent the 50th and 75th percentile grouping. As indicated in Table II, most of the measurement data for the computer models varies somewhat between these two groupings, but tends toward the 50th percentile grouping. Bodily regions, as described in the models, are consistent with those defined in the currently accepted "computer man" model developed by the Research Division of Chemical Systems Laboratory at Edgewood. The calculation of the weight for the computer models is based on MOMENT Subroutine calculations for the total volume of the computer models. Details regarding weight calculations are discussed in the following section and Appendix A.

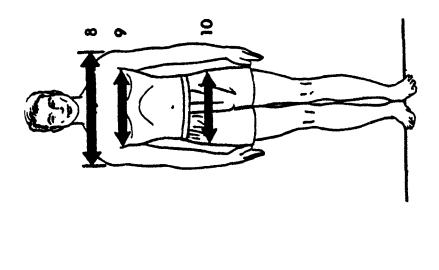
The origin of the coordinate system used for these models are located within the heads of the models, at a point centered between the eyes, the forehead, and the rear of the head; it is located 48.26 millimetres (mm) (1.9 inches) above the eyes. Figure 4 and 6 display the front and side views of the graphical representatives of the models of sitting and standing man, respectively, complete with location of the center of their coordinate system and direction of the positive coordinate axis. The height of the center of coordinates is also shown. Figures 5 and 7 display the front and rear oblique views of these models, indicating additional detail. Dimensions pertinent to the space or volume required for emplacement of these models within a weapon or target system model can be obtained from Table II. Two versions of the models of sitting and standing man were prepared, helmeted and unhelmeted. The helmeted version of sitting man contains 56 solids and regions. while the unhelmeted version contains 50. Similarly, the helmeted version of standing man contains 62 solids and regions, while the unhelmeted version contains 56. Consistent with the units of measure. It used in both past and current weapon system models, the crew personnel are available in either inch or millimetre dimensions.

IV. VALIDATION PROCEDURE

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The validation procedure entails a series of steps which are designed to verify that the COM-GEOM computer models are correctly prepared, that is, valid. The series of steps begins with the application of the CHECK Subroutine of the GIFT computer code. The CHECK Subroutine determines whether regions overlap, that is, occupy the same volume within the computer model. A $\hat{v}.25$ mm allowable overlap tolerance, defined as the maximum amount which the components can overlap, was used in the CHECK analysis of these models. Overlaps noted by this step were subsequently corrected.

Robert M. White, "The Body Size of Soldiers; US Army Anthropometry - 1976," US Army Natick Laboratories Technical Report No. 72-51-CE, December, 1971.



• 7

8. Shoulder Width 9. Chest Width 10. Hip Width, Standing Waist Height
 Crotch Height
 Kneecap Height
 Chest Depth

Stature Height
 Cervical Height
 Shoulder Height

Numerical Indices for Various Measurements Taken from Actual Standing US Army Soldiers Figure 2.

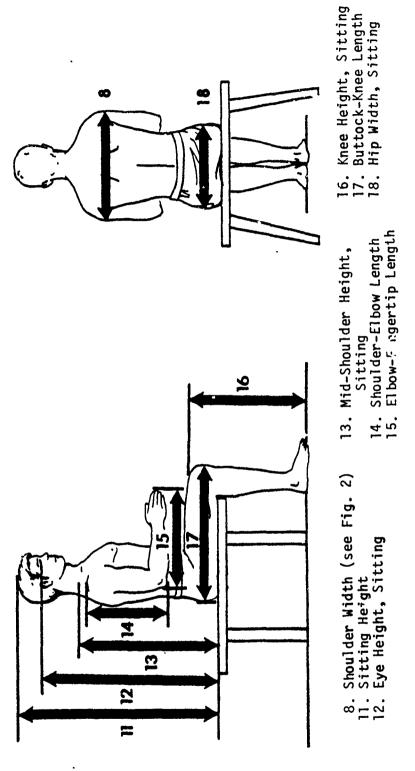


Figure 3. Numerical Indices for Various Measurements Taken from Actual Sitting US Army Personnel

Comparison of Anthropometric Measurements from US Army Soldiers and Measurements from Computer Models of Sitting and Standing Personnel Table II.

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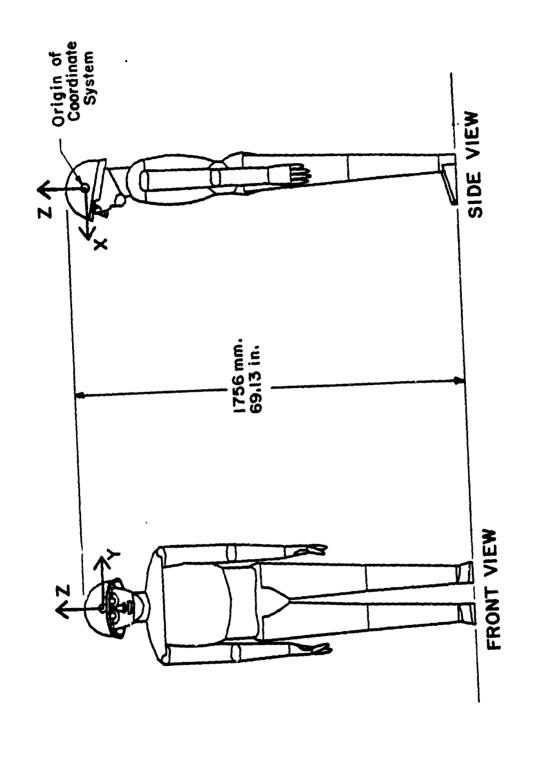
	Measurement Type	-		Measurement Data	Measurement Data [millimetres (inches)]	_	
	1	Soth P	th Percentile	Comput	Computer Models	75th Per	75th Percentile
Ind	Index Description	Sol	Soldier	Standing	Sitting	Soldier	lier
•	Weight ²	7.07	(156)	72.12 (159)	75.60 (167)	78.47	(173)
1	Stature Height	1745	(68.7)	1756 (69.1)	1773 (69.8) ³	1788	(70.4)
C1	Cervical Height	1494	(58.8)	1488 (58.6)	† - 	1539	(9.09)
153	Shoulder Height	1438	(56.6)	1445 (56.9)	\$ 1 9 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	1478	(58.2)
4	Waist Height	1064	(41.9)	1036 (40.8)	1 1 1 1 1	1102	(43.4)
S	Crotch Height	838	(33.0)	828 (32.6)	1 1 1 1	871	(34.3)
9	Kneecap Height	528	(20.8)	~508 (20.0)	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	551	(21.7)
7	Chest Depth	231	(9.1)	216 (8.5)	1 1	244	(9.6)
∞	Shoulder Width	452	(17.8)	508 (20.0)	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	470	(18.5)
6	Chest Width	305	(12.0)	356 (14.0)	1 1 1	320	(12.6)
10	Hip Width, Standing	330	(13.0)	338 (13.3)	# 2	345	(13.6)
11	Sitting Height	206	(35.7)	1 1 1 1 1	904 (35.6)	932	(36.7)
12	Eye Height, Sitting	787	(31.0)	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	792 (31.2)	813	(32.0)
13	Mid-Shoulder Height Sitting	525	(24.6)	1	638 (25.1)	645	(25.4)
14	Shoulder-Elbow Length	368	(14.5)	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	~356 (14.0)	381	(15.0)
15	Elbow-Fingertip Length	478	(18.8)	429 (16.9)	351 (13.8)	495	(19.5)
16	Knee Height, Sitting	541	(21.3)	1 1 1 1	556 (21.9)	529	(22.0)
17	Buttock-Knee Length	594	(23.4)	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	597 (23.5)	612	(24.1)
18	Hip Width, Sitting	340	(13.4)	1 1 1 1	356 (14.0)	356	(14.0)

¹ See Figures 2 and 3

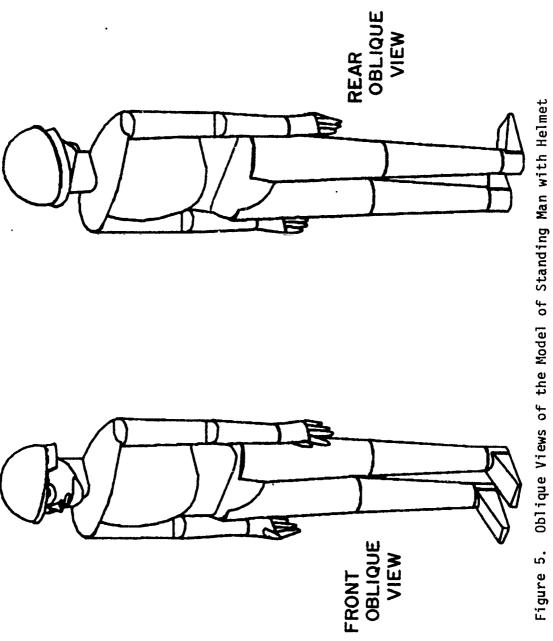
 $^{^2}$ Weight is stated in units of kilograms and pounds ().

 $^{^3}$ This is the height of Sitting Man if he were erected to a standing position.

 $^{^4}$ Hand is in a clenched position.



Front and Side Views of the Model of Standing Man with Helmet Showing Orientation and Origin of Coordinate System Figure 4.



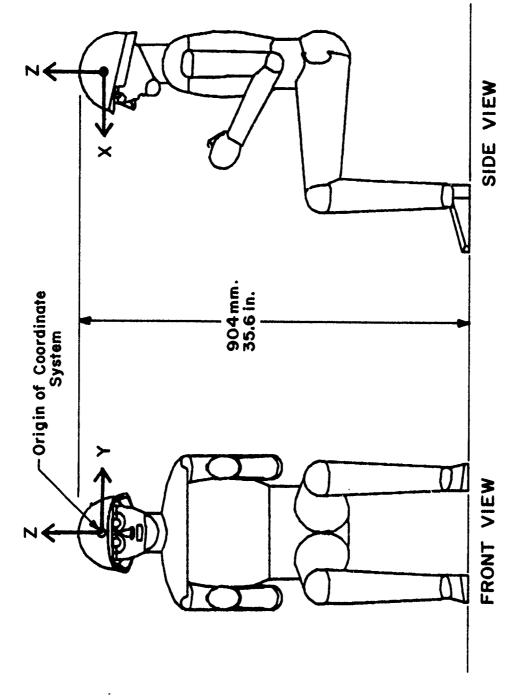
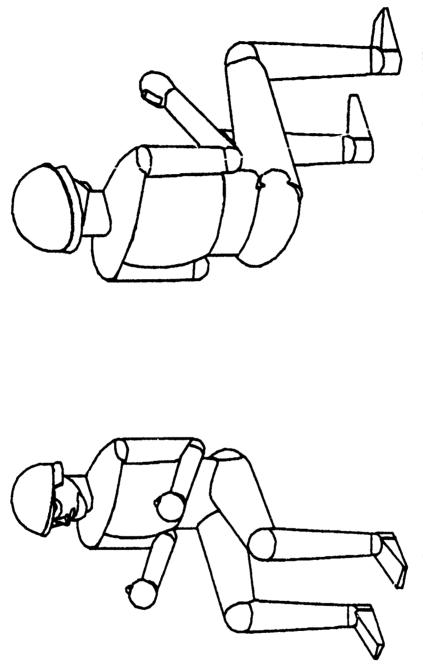


Figure 6. Front and Side Views of the Model of Sitting Man with Helmet Showing Orientation and Origin of Coordinates



FRONT OBLIQUE VIEW

REAR OBLIQUE VIEW

Figure 7. Oblique Views of the Model of Sitting Man with Helmet

The second step of the validation procedure uses the GRID Subroutine to determine whether unwanted voids or undefined volumes exist in the computer model; it does this by examining the model in fine detail from various directions. The GRID Subroutine passes a plane, which is perpendicular to the attack aspect under consideration, through the origin of the computer model's coordinate system. A grid overlay is then superimposed on this plane and for each cell on this grid overlay, a ray, normal to the attack plane, is projected through the computer model. As each ray is traced through the computer model, LOS thickness, normal thicknesses, and the obliquity angles are enumerated for every Item encountered along the ray path. Voids highlighted by this step are then corrected.

A third step in the validation procedure involves the use of the MOMENT Subroutine of the GIFT computer code. The MOMENT Subroutine also projects rays through the model but with the intent of producing estimates of weights of components based on individual component (Item) densities. Moments of inertia along with total weight and volume of the model are also calculated in this subroutine. The component (Item) densities are the key input data in exercising the MOMENT Subroutine; calculations of all other values are dependent on the accuracy of these data. However, often exact density values are not available because the component is comprised of more than one material (non-homogeneous) or it has a shape or volume that is irregular. In the case of components having internal air spaces, LOS percentages of solid material to air must be considered; this determines how the density must be "adjusted" to correctly calculate a total component weight. The analyst adjusts the density on successive computer runs so that the individual component weights correspond, within a desired tolerance, to their actual weights.

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Since there are no density values available for the individual body regions, as defined in these models, an average density of 1.07 gm/cm³ was initially used for all of the body components. (The density of 1.07 gm/cm³ is the accepted density value for soft tissue of the human body.) Analysis of the MOMENT output data, using densities of 1.07 gm/cm³, indicated that, for the volume and height, the models of the sitting and standing crew personnel were too light in weight. Subsequently, it was determined that the average density used for the personnel models was not large enough and a new algorithm, based on the density of soft tissue and bone, should be used. This algorithm, derived in Appendix A is based primarily on the percentage values, by weight, of bone and muscle within an average human body and the total body volume as calculated by the MOMENT Subroutine. The total weights and final "adjusted" density values used for all the components of sitting and standing man as calculated by this new algorithm are as follows:

	Density (gm/cm^3)	Body Weight (kg)
For Sitting Man	1.1843	75.60 (167 lbs)
For Standing Man	1.1794	72.12 (159 1bs)

Using these density values, the total weights were verified by the MOMENT Subroutine. The differences in the body densities and weights, shown above, are accounted for by the slight differences in the total body volumes of the sitting and standing personnel models as calculated by the MOMENT Subroutine.

Another step in the validation procedure consists of the generation of computer graphic illustrations of the model, as produced by the PICTUR Subroutine of the GIFT computer code. These computer illustrations are examined in detail to determine if all regions are in their proper position. Figures 4 through 7 represent computer illustrations produced by the PICTUR Subroutine.

V. MODEL UTILIZATION INFORMATION

The computer models of sitting and standing crew personnel were constructed so that the geometric solids comprising the arm and legs could be moved selectively into more realistic positions, if required. To facilitate any required movement (rotation) of geometric solids, pivot points corresponding to various body joints were designated. However, in regard to the pivot points, the models of sitting and standing man are slightly different: only the model of sitting man has knee and ankle joints. Pivot points and their coordinate values are listed for both models in Table III. Body positions involving the movement of the back (either bends or twists) have not been designed for the models.

The validated computer models of sitting and standing crew personnel are available in English (inch) and metric (millimetre) dimensions and are currently accessible on the CYBER 76 computer. The authors express sincerely the opinion that the use of these models of crew personnel will enhance and increase the credibility of current weapon or target system models.

Table III. Coordinates of Selected Pivot Foints Within Models of Sitting and Standing Crew Personnel.

Description of Pivot Point Base of Neck (for head movements) Shoulders (shoulder joint) Elbows Hips (base end of thigh) Knees	Siffil X -25,40 -25,40 -44,45 407,35	X, Y B Sitting Crewman Y O 0.0	Z Values For 2 2 -241.30 -292.10 -777.85 -746.13 -746.13 -1168.40	X, Y & Z Values For Pivot Points (mm) Y X X X X X Co241.30 -25.40	Standing Crewman Y 0 0.0 0 ±209.55 0 ±215.90 0 ±84.14	2 -241.30 -292.10 -609.60
Knees Ankles	407.35	±178,42 ±178,42	-746.13		, ,	
Hips (base end of thigh)	-44.45	±69,85	-746.13	-38,10	+84.14	-739.38
Elbows	-25,40	±215,90	-577,85	-25,40	±215,90	09'609-
Shoulders (shoulder joint)	-25,40	±209,55	-292,10	-25,40	±209.55	-292.10
Base of Neck (for head movements)	-25,40	0.0	-241, 30	-25,40	0.0	-241.30
		Y	i	- 11	\	
Description of Application Point	Sittle	ng Crewman		Star	iding Crewma	ci
	***************************************	x, ≺	Z Values For	· Pivot Points ((ww	

ACKNOWLEDGMENT

The authors gratefully acknowledge the contributions of Mr. David Neades, for the data he furnished and for the discussions which led to the analysis within Appendix A.

APPENDIX A

CALCULATION OF "ADJUSTED" WEIGHT AND DENSITY OF THE CREW PERSONNEL MODELS

CALCULATION OF ADJUSTED WEIGHT AND DENSITY OF THE CREW PERSONNEL MODELS

(Based on the Volumes Computed by MOMENT Subroutine)

Initially, if one makes the assumption that the human body is comprised basically of two kinds of tissue, bone and soft tissue (which includes all the muscles, internal organs, etc.), then, the total volume of the human body $(V_{\mbox{\scriptsize HB}})^1$ can be expressed as the volume of bone $(V_{\mbox{\scriptsize B}})$ plus the volume of soft tissue $(V_{\mbox{\scriptsize ST}})$. This relationship is shown as:

$$V_{HB} = V_B + V_{ST} \tag{1}$$

The MOMENT Subroutine computed only V_{HB} ; V_{B} and V_{ST} are not known and must be determined from other quantities.

$$V_{HR}$$
 (for sitting man) = 63835.05 cm³ (2.2543 ft³)

$$V_{HB}$$
 (for standing man) = 61147.76 cm³ (2.1594 ft³)

The total weight of the human body (W_{HB}) is expressed as the weight of bone (W_B) plus the weight of soft tissue (W_{ST}) , or

$$W_{HB} = W_B + W_{ST}. \tag{2}$$

However, the percent of bone by weight 2 in an average adult human body is a known quantity and may be used as the basis for determining W_{HB} ,

% Bone_{HB} =
$$\frac{W_B}{W_{HB}}$$
 = 43 (3)

and

% Soft Tissue_{HB} =
$$\frac{W_{ST}}{W_{HB}}$$
 = 57. (4)

¹Subscripts B, ST, and HB represent Bone, Soft Tissue, and Human Body, respectively. They are used throughout the appendix.

The percent of bone by weight in an average human body determined to be 43%. Ref: Dave Neades (undisclosed source).

 $\mathbf{W}_{\mathrm{HB}}\text{, }\mathbf{W}_{\mathrm{B}}\text{, and }\mathbf{W}_{\mathrm{ST}}$ are, at this point, undetermined; but

$$W_B = V_B \rho_B$$

and

where

 $\rho_B = 1.8 \text{ gm/cm}^3$

(This represents an average from a range of densities between 1.7 - 2.0 gm/cm³.)

and

 $\rho_{ST} = 1.07 \text{ gm/cm}^3$.

Therefore,

$$W_B = 1.8 \text{ gm/cm}^3 \text{ V}_B$$

and

$$W_{ST} = 1.07 \text{ gm/cm}^3 \text{ V}_{ST}.$$

Substituting for $\mathbf{W}_{\mathbf{B}}$ and $\mathbf{W}_{\mathbf{ST}}$ from Equations 3 and 4 produces:

$$0.43 W_{HB} = 1.8 gm/cm^3 V_B$$
 (5)

and

0.57
$$W_{HB} = 1.07 \text{ gm/cm}^3 V_S$$
. (6)

Since $V_{HB} = V_B + V_{ST}$ (Equation 1), Equation 5 and 6 must be divided by 1.8 gm/cm³ and 1.07 gm/cm³, respectively, or

0.2389 gm/cm³
$$W_{HB} = V_B$$
 (7)

and

0.5327 gm/cm³
$$W_{HB} = V_{ST}$$
. (8)

Adding Equation 7 and 8 yields

0.7716 gm/cm³
$$W_{HB} = V_{HB}$$
; (9)

but, knowing that

$$V_{HB}$$
 (for sitting man) = 63835.05 cm³

and

$$V_{HB}$$
 (for standing man) = 61147.76 cm³,

we can substitute in Equation 9 and determine that

$$W_{HB}$$
 (Sitting Man) = $\frac{63835.05 \text{ cm}^3}{0.7715 \text{ cm}}$ = 82.73075 Kg (182.39 1b)

and

$$W_{HB}$$
 (Standing Man) = $\frac{61147.76 \text{ cm}^3}{0.7716 \text{ gm}}$ = 79.24800 Kg (174.412 lb)

Consequently, substituting the values of $W_{\mbox{HB}}$ into Equations 7 and 8 respectively, yields (for sitting man):

$$V_{R} = (0.2389 \text{ gm/cm}^3) (82730.75 \text{ gm}) = 19764.38 \text{ cm}^3$$

and

$$V_{ST} = (0.5327 \text{ gm/cm}^3) (82730.75 \text{ gm}) = 44070.67 \text{ cm}^3;$$

and (for standing man):

$$V_{R} = (0.2389 \text{ gm/cm}^3) (79248.00 \text{ gm}) = 18932.35 \text{ cm}^3$$

and

$$V_{ST} = (0.5327 \text{ gm/cm}^3) (79248.00 \text{ gm}) = 42215.41 \text{ cm}^3.$$

For the sitting man the % bone by volume, using Equation 1 is

$$\frac{V_B}{V_{HB}} = \frac{19764.38 \text{ cm}^3}{63835.05 \text{ cm}^3} = 0.3096 \text{ or } 30.96 \%$$

the % soft tissue by volume (also using Equation 1) is

$$\frac{V_{ST}}{V_{HB}} = \frac{44070.67 \text{ cm}^3}{63835.05 \text{ cm}^3} = 0.6904 \text{ or } 69.04 \text{ %}.$$

The same percentages hold true for the standing man:

$$\frac{V_B}{V_{HB}} = \frac{18932.85 \text{ cm}^3}{61147.76 \text{ cm}^3} = 0.3096 \text{ or } 30.96 \%$$

and

$$\frac{V_{ST}}{V_{HB}} = \frac{42215.41 \text{ cm}^3}{61147.76 \text{ cm}^3} = 0.6904 \text{ or } 69.04 \%.$$

It is now possible to develop an average density of the human body, \bar{o}_{HB} , which can ultimately be used with modifications in the MOMENT Subroutine of GIFT program to calculate the total body weight, W_{HB} .

Since individual component densities are not available for the individual components as defined, average density, ρ_{HB} , is multiplied by <u>all</u> components volumes calculated by the MOMENT Subroutine.

The average density, $\bar{\rho}_{HB}$, based on volume considerations, can be computed as follows:

$$\bar{\rho}_{HB} = X \rho_B + Y \rho_{ST}$$

where: $X = V_B / V_{HB} = 0.3096$, $Y = V_{ST} / V_{HB} \approx 0.6904$, $\rho_B = 1.8 \text{ gm/cm}^3$, and $\rho_{ST} = 1.07 \text{ gm/cm}^3$.

$$\bar{\rho}_{HB} = (0.3096) (1.8 \text{ gm/cm}^3) + (0.6904) (1.07 \text{ gm/cm}^3)$$

$$= 0.5573 \text{ gm/cm}^3 + 0.7387 \text{ gm/cm}^3$$

$$\bar{\rho}_{HB} = 1.296 \text{ gm/cm}^3$$

This can be verified by rearranging Equation 9

$$0.7716 \text{ cm}^3/\text{gm W}_{HB} = V_{HB}$$

Since $W_{HB} = \bar{o}_{HB} V_{HB}$, we find that

$$\bar{\rho}_{HB} = \frac{1}{0.7716} \text{ cm}^3/\text{gm or } 1.296 \text{ gm/cm}^3$$

To be more precise in the weight calculations, the volume of air in an average set of lungs, 3 V_L, was subtracted from the total body volume, V_{HB}, to yield an "adjusted" body volume (V_{HB} - V_L). The "adjusted" body volume was multiplied by the average body density, $\bar{\rho}_{HB}$, to produce the "adjusted" body weight, W_{HB}. In equation form, this is written as follows:

$$W_{HB} = \bar{\rho}_{HB} (V_{HB} - V_L)$$

where: $\bar{\rho}_{HB} = 1.296 \text{ gm/cm}^3$, $V_{HB} = 63835.05 \text{ cm}^3$, and $V_L = 5500 \text{ cm}^3$,

$$W_{HB} = 1.296 \text{ gm/cm}^3 (58335.05 \text{ cm}^3)$$

(for sitting man)

$$W_{HB} = 75.60222 \text{ kg (166.67 1b)}$$

$$W_{HR} = \bar{\rho}_{HR} (V_{HR} - V_{L})$$

where: $\bar{\rho}_{HB} = 1.296 \text{ gm/cm}^3$, $V_{HB} = 61147.76 \text{ cm}^3$, and $V_L = 5500 \text{ cm}^3$,

$$W_{HB} = 1.296 \text{ gm/cm}^3 (55647.76 \text{ cm}^3)$$

(for standing man)

Since the volume of air in the lungs, V_L , is not recounted for in the models because of the way they are constructed, the average body volume, V_{HB} , (which is calculated by the MOMENT Subroutine) is used with the "adjusted" body weight, W_{HB} , to develop a corrected average human body density, $\bar{\rho}_{HB}$. This is calculated using the following equation:

The "average" lung capacity, from deepest inspiration to deepest expiration, of a twenty year old male, approximately 1778 mm (70 inches) in height, is 5500 cm³. Source: Civilian Employees Health Clinic Data.

For sitting man:

$$\bar{\rho}_{HB} = \frac{W_{HB}}{V_{HB}}$$

where: $W_{HB} = 75602.22$ gm and $V_{HB} = 63835.05$ cm³,

$$\bar{\rho}_{HB} = \frac{75602.22 \text{ gm}}{63835.05 \text{ cm}^3}$$

$$\bar{\rho}_{HB} = 1.1843 \text{ gm/cm}^3$$

For standing man:

$$\bar{\rho}_{HB}' = \frac{W_{HB}'}{V_{HB}}$$

where: $W_{HB} = 72119.50 \text{ gm} \text{ and } V_{HB} = 61147.76 \text{ cm}^3$,

$$\tilde{\rho}_{HB}' = \frac{72119.50 \text{ gm}}{61147.76}$$

$$\bar{\rho}_{HB} = 1.1794 \text{ gm/cm}^3$$

If density is an important parameter in determining ballistic resistance of a human body to penetrating mechanisms in a typical weapon system vulnerability study, perhaps the analyst should consider using the "adjusted" average body density $\bar{\rho}_{HB} = 1.18$ gm/cm³ rather than just the value for soft tissue, 1.07 gm/cm³, per se. With reference to the initial assumption that the human body is comprised basically of two kinds of tissue - bony and soft, it is recognized an "adjusted" density does not always represent reality when it comes to calculating human body resistance to penetrating mechanisms. A feasible way around this situation is to construct human models with internal skeletons so that resistance of bone and soft tissue can be distinguished; however, the significance of this approach remains undetermined.

APPENDIX B

TABULATION OF COM-GEOM DATA FOR MODEL OF SITTING CREW PERSONNEL (WITH HELMET)

TABLE B-I. GEOMETRIC SOLIDS COMPRISING COMPUTER MODEL OF SITTING CREW PERSONNEL

REMARKS	HEAD TOP	HEAD MID	HEAD LOWER	NECK	NOSE TOP	NOSE LOWER	A 11 GT SON		JAW - CHIN	Z P A S S		LEFT EY	RIGHT EYE	LFT DUTE) -LFT EAR		RGT OUTEAR		-RGI EAR	1	SOCKET
	0.000	.100	0000	139.700	55.8800	000	6.3500	.620	.960	9.210	.850	0.000	0.000	7.940	.940	8.669	27.940	8.669	7.940	8.669	8 8 9 •
	000	000			0.0000	000000	0000	000	.000	000	000	.000	00000	.510	.372	9.372	6.510	-9.372	6.510	.372	0.800
AMETERS	. 600	000	101.6000		-12.7000	130	0-	000.0	8.420	.480	000.0	0.320	0.320	5.400	.427	14.427	25.400	4.427	25.400	14.427	9.210
SOLID PAR	7000	.800	-50.8000	300	-106.6800	089.	0 4	00000	.000	.000	00000	.260	.260	7.150	99	0.000	.150	00000	.960	00000	. 800
	000	000		0.000	0000		2.0	0.320	0.000	3.500	1.280	5.400	5.400	8.900	21.2852 93.9800	1.285	8.900	1.285	3.980	1.285	8.260
	0000	0000			.060	7 1 0	0.000	0.000	.700	000	000	3.500	.500	000.0	. 843	.843	000.0	. 843	. 080	13.843	.084
SOLID NUM TYPE	1 ELLG	2 REC	3 ELLG	4 RCC	5 TEC	6 F11 G		, בררפ	8 ELLG	0	1 1	O SP	11 SPH	2 EL	13 ELLG		14 ELLG		15 ELLG		16 ELL1

TABLE B-I. GEOMETRIC SOLIDS COMPRISING COMPUTER MODEL OF SITTING CREW PERSONNEL (CONTINUED)

REMARKS	RGT EYE	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		FOR HOTOP	RHEL		NNRHEL M1	;	DUTRHELM2)		NNRHEL M2			HEIM SECT		HELM SEC2	:			SHOULDERS	: } !	HOULDER)		14.	ARM	SHOULDER	JOINT
_	- 00000 •0	1 004	0.000	- 00000	0000	0800	0.000.0	9.3800	31,1277	0000-0		.1277 I	0000)))	2.8648 -	83,1952	35.5600 -	.3300	35.56	9.38	0.0000	.0000	9.7000 -	54.0000 T	0000	.7500 L	0000	00	. 7500
	50.8000	.000	.800	3.200	0	000	.000	000	000	.330		0	118.6307	! !	000	000	52.400	52.400	52.400	52.400	254.0000	00000	.100	.000	.000	.3500	.000	000	00
ARANETERS	29.2100	.875	8	7.000	Ň	00	.840	.000	96	• 000		-7.4905	00.		-41.5976	45.	2	38.	2	8	000000	91.5480	•	•	107.7341	•	44.4500	44.4500	0
SOLID PAR	-50.8000	5.2	73.660	.700	0.80	000	.800	8	.927	.388		81.	0.337		-182.0672	•	•	•	6	8	-292.1000	•	•	•	00000	-292.1000	0.0000	-292.1000	0.000
	-48.2600	4.	o	•	0.000	•	Ö	•	•	•		0.000.0			52.	04.	52.	•	52.	52.	000000	0	•	ċ	ċ	209.5500	÷	.550	44.4500
	111.7600	2.240	29.540	39.700	90.	900	90.	.000	7.490	. 696	? !	7.490	.075	8	.462	000.	0.800	. 800	0.800	7.800	5.400	000.0	27.000	5.400	000.	. 400	000	-25.4000	• 000
SOLID NUM TYPE	17 6411	18 RAW		19 RPP	O EL		21 ELLG		22 TEC		1	23 IEC			24 BOX		25 ARB8				56 ELLG		Ō.	8 EL		29 TEC		30 ELLG	

TABLE B-I. GEOMETRIC SOLIDS COMPRISING COMPUTER MODEL OF SITTING CREW PERSONNEL (CONTINUED)

The second of th

REMARKS	R IGHT ARM	RTSHOULDER JOINT LEFT	FOREARM LEFT ELBOW RIGHT FORFARM	TEL	EFT EFT SEC	RIGHT FIST RGHT THUMB RGHT THUMB SEC 2	DOM	LEFT THIGH LEFT KNEE LEFT
	-285.7500	0.0000 31.7500 132.0800	0.0000		0.000	-46.1823 0.0000 0.0000 -44.4195	203.2000	0.00 0.00 22.27
	-6.3500	000000000000000000000000000000000000000	000000000000000000000000000000000000000	0.0000	000.0	38.1000 0.0000 0.0000	000000000000000000000000000000000000000	0000
AMETERS	0.0000	44.4500 0.0000 254.0000	38.1000	38.1000 21.1633 0.0000	2.700	21.1633 0.0000 12.7000 -26.1849	0.0000 82.1233 88.9000	150
SOLID PAR	-292.1000	-292.1000 0.0000 -577.8500	-577.8500	7.8505.688	369.509	-415.6888 26.4541 -369.5090 -369.5090	0.0000-774-7900	22 22 23 25 25 25
	-209.5500	.55. .45	31.7	666	15.90	-215.9000 0.0000 -215.9000	0000	69.8500 57.1500 178.4172 178.4172
	000	5.400 0.000 5.400	8.100 5.400 6.400	25.400 57.787 57.787	36.626 36.626 12.700	. 787 . 726 . 626 . 626	4.000 0.000 0.000 0.000	-44.4500 95.2500 407.3474 407.3474 57.1500
OLIO IM TYPE	1 TEC .	12 ELLG 13 TRC	4 SP 5 TR	16 SPH	8 SPH 9 RCC	O ELLG	3 REC	5 TRC 6 SPH 7 TRC
N UN	m	ന ന	mm	നന	<i>.</i> .	4 44	4 4	4 44

TABLE B-I. GEOMETRIC SOLIDS COMPRISING COMPUTER MODEL OF SITTING CREW PERSONNEL (CONTINUED)

C	-							
N O N	TYPE			SOLID PAR	PARAMETERS			REMARKS
8 4	TRC	-44.4500	-69.8500	-746.1250	451.7974	-108.5672	0000000	R IGHT TH IGH
	٩	7.347	-178.4172	•	57.1500	0.0000	0.0000	IGH
20	TRC	7.347	-178.4172	1	000000	0.000	-422.2750	· -
		7.150	38.1000					LEG
51	RCC	7.347	178.4172	-1244.6030	00000	0.000	76.2000	LEFT ANKLE
	٥	7.347	7	-1168,4000	38,1000	0000	0000	
) (N)		7.347	-178.4172	-1244.6000	0000	0000	76.2000	RGE I
	1	8.100						
	۹.	7.347	78.417	-1168.4000	38.1000	000000	0.0000	RTANKPIVOT
55	ARB8	3.971	29.217	-1244.6000	7	140.3172	9009	LEFT
		1.497	40.317	-1219.2000	9	٠.	9000	FOOT
		3.697	16.517	-1244.6000	3.	٠.		
		3.697	140.3172	-1168.4000	413.6974	216.5172	-1183.5765	
56	ARB8	3.971	229.217	-1244.6000	Ή.			RIGHT
		1.497	40.317	-1219.2000	573.9714	•	-1231.9000	F001
		3.697	216.517	-1244.6000	3		60	
		3.697	40.317	-1168.4000	413.6974	-216.5172	-1183.5765	

TABLE 8-II. REGION COMBINATION TABLE FOR KODEL OF SITTING CREW PERSONNEL

REMARKS	HEAD TOP HEAD MIDDLE -11 HEAD LOWER	NECK NOSE NOSE NOSE CHIN			FEAR RT EA		UPRSE	LWRS TELM TELM	DERS SHOUL	AX ADU	RIGHT ARM
	-10										
REGION COMBINATION DATA	Ŷ									64-	
	-11			-23	-23				-32	-32	
	-10 -18		-17	-21	-21				-31	-31	
REGION C	-9	-26 -7 -7	-16	£ 3	1 3			-25	-30	130	-36
	-9 -17 -16	111	-11	-2	-2		-24	24	-29	129	-35
				-13	-15		-21	-23	27	-27	-32
zα	-	4 W O L O	6 O H		14		20	22	26	2	
REGION	N E	40000	6 0 H	7 5 7	17	16 17 18 19	20	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	26 27 27	28 29 30	31

TABLE 8-II. REGION COMBINATION TABLE FOR MODEL OF SITTING CREW PERSONNEL (CONTINUED)

REMARKS	RT SHOULDJI LT FOREARM	RT FOREARM	LEFT FIST LT THB SC1	RIGHT FIST RT THB SCI	ABDONEN PELVIS FFT THIGH	LEFT KNEE LEFT LEG RIGHT THIGH	RIGHI KNEE RIGHT LEG LEFT ANKLE	RIGHT ANKLE RT ANKLE JT LEFT FOOT RIGHT FOOT
COMBINATION DATA								
REGION			-39	-45	1 1 84 4	-52	-54	
			8 6 1	-41	1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	151	1 1 55 55 55	- 56
	-34	-36	-33 -39	135	111	96	-49	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	ώ ω ς Μ ω γ	0 60 4 5 10 4) F & 0	, 6 4 4 0 11 0 4	ተ ቀ ቀላ ነጥ ቀ ሆ	9744	4 10 10 10 0 11 0	ነ ለነ የነ የነ የ መ ዱ የህ ብ
REGION NUMBER	288	ህ ሠ ሂ ት የህ ሊ		, 4 4 4 0 H 6	ተቀቀላ ባጠቀሆ	1010	4 0 0 1 0 1 0	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7

TABLE B-III. REGION IDENTIFICATION TABLE FOR MODEL

	LOS PERCENT	100				25	25	25		100				(100					•	100		100			(100	•	001	100	100	001
	MATERIAL Code	81													60 80					į	7.7	(7.7				87	Ġ	x 0	Ф (o∙ (Ď
OF SITTING CREW PERSONNEL	DESCRIPTION	OF HEAD - SKULL	IDDLE OF HEAD - SK	OTTOM OF HEAD - SKUL	EC	OSE - UPP	OSE - LOWE	OSTRIL	OWER J	BRAIN	EFT E	RIGHT EYE	EFT EAR	-DUMMY	ď	RIGHT EAR	LEFT EY	RIGHT EYE SOCK	(SHAPES MOUTH	HEAD TOP	IPPER SECTION	-DUMNY HELNET	LOWER SECTION	-DUMMY HELMET (INSIDE SECTION 2)	HELMET (SHAPES SECTION I	-DUMMY HELMET (SHAPES SECTION 2	JLDERS	WDQ-	HORAX	EFT ARM	早S 14	RIGH! ARM
 	SPACE CODE																															
	ITEM	.	-	-	2	m	m	ო	4	ß	9	•	7	111		_	-	\vdash	111	-		111		111	H	-	Φ	111				11
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APPENDIX C

TABULATION OF COM-GEOM DATA FOR MODEL OF STANDING CREW PERSONNEL (WITH HELMET)

TABLE C-I. GEOMETRIC SOLIDS COMPRISING COMPUTER MODEL OF STANDING CREW PERSONNEL

EM ARK S	AD. TOP	AD MID		AD LOWER		Λ X		SE TOP			SE LOWER		OSTRILS		M - CHIN		AIN		T EY	GHT EYE	OUTE		FT EAR		T OUTEAR		GT EAR		FT EYE	CKE
œ	9 H	O HE	0	O HE	0	O NE			0		ON O	0	z	9	10 JA	0	00 BR	0	0	O RI	0	o	7-0	0	O RG	0	0 -R	0	7-0	Ś
	0.000	.10	00.	0.00	39.70	.70		. 88	0		.00	.35	00000	.62	0.96	.21	0.00	.85	.00	.00	7.94	• 66	7.94	8.66	7.94	8.66	7.94	8.66	.00	•
	0.0000	0.000	.900	.000	000.	.000		•000	15.2400		.000	.000	0.0000	.000	000	.000	.000	000	.000	0000	.510	9.372	.510	.372	6.510	.372	6.510	9.372	0.800	
AMETERS	101.6000	.000	0.000	. 600	000.	000.		. 700	0		i i	000.	21.5900	.000	8.420	.480	2.710	.000	0.320	.320	25.400	4.427	25.400	14.427	25.400	14.427	5.400	14.427	9.210	
SOLID PAR	-12.7000	.800	.000	.800	000	.300		80	0.000		80	.000	-104.1400	.000	.000	000.	9	•000	8.260	.260	7.150	.000	096.	000	.150	000.	•960	0000	.800	
	0.0000	.000	• 000	000	.900	.000		.000	000000		.000	.240	000000	.320	.00c	.500	.000	1.280	5.400	.400	8.900	1.285	3.980	1.285	3.900	1.285	3.980	1.285	8.260	
	0.0000	000.0	• 600	.000	000	. 400	3.500	9.060	5.400	1.666	.060	0.000	.250	.000	.700	.000	.000	.000	.500	3.500	0.000	.843	• 080	.843	000	.843	.080	13,843	.760	7.084
ID TYPE	ELLG	REC		ELLG		RCC		TEC			ELLG		ELLG		ELLG		ELLG		٥	SPH			ELLG		ELLG		ELLG		ELL1	
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TABLE C-I. GEOMETRIC SOLIDS COMPRISING COMPUTER MODEL OF STANDING CREW PERSONNEL (CONTINUED)

SOLID NUM TY	.ID TYPE			SOLID PARAMET	METERS			AARK
17	ELL1 .	-	-48.2600	-50.8000	29.2100	50.8000	000000	RGT EYE SOCKET
	•	37.	604	20	.875	000	27.9400	-FOR MOUTH
18	KAK	7 • 7 • T	000	73.660	0.00	50.800	0000	1011
	•	100	700	39.700	27.000	3.200	0000	FICK BUILDE
61	¥ .	0,0	; 0	-50.8000	129.5400	0.000	0000.0	_
	ר		380	00000	00000	000	000	T N 100 UNI W1
		•	000	.800	. 840	000		MARTICE
77	בורפ		680	0.000	. 000	000	9860	CM ISHOTION
	u		0000	27	. 490	0000	11711	;
77	ر ا		000	.337	000	330	•	
		7		(•		1277	I NNRHEL M2
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	j	_	000000	m.	•	0000	•	
		-		1			2 BEER	-HFLM SECT
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1	0	ċ	04.800	0	5.729	000.0	74 OCO	CJES M SECS
	•	, ,	52.400	9	52.400	52.400		מור חור
7	AKDO	•	2.400	6.8	8.100	52.400	74. 50	
		- 4	52.400	9.0	400	152.400	, 0	
		100	152,400	0	38.100	52.400	19.38	
	į			7	0.000	54.000	ö	SHOOLDER
56	ELLG	•		88.9	1.948	80.	0	
	(֖֭֭֭֓֞֝֞֜֜֓֓֓֓֓֓֓֓֓֡֜֜֝֓֡֓֡֓֡֓֡֓֡֓֡֓֡֓֡֓֡֡֡֓֡֓֡֡֡֓֡֡		6.7	266.7000	100	-139.7000	-SHOULDER
27	X 9 .			410.1	0.000	900	54.00	IHUXAX
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		ċ	2000	֓֞֜֜֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֓֓֡֓֡֓֡֓	00'00	.350	.5	LEFT
29) TGC	-25.4000	204.5500	0000-0	*	000000		ARM
			0000	•		,		101101
,	L	•	9.550	-292.1000	44.4500	000000	00000	LISAUGLUER
9	ה ה		44.45	8	0	000.		•

TABLE C-I. GEOMETRIC SOLIDS COMPRISING COMPUTER MODEL OF STANDING CREW PERSONNEL (CONTINUED)

REMARKS	IGHT ARM	S	EFT FOREARM	EFT ELBOW		IGHTEL BOW	. ∢	FTHUM	H OH	INGER	INGER T THIRD		uu	1
	-317.5000 R 0.0000	.000	-241.3000 L 0.0000	0.0000 L	0000 • 0	0.0000 R	000000	.413	.200	0.0000	0.0000	.000	-508.0600 - -101.6000 R	•
	0.0000	000	0.0000	0.0000	000	0.0000	00000	0.000	900	0000	000	000	-952.5000 -12.7000 0.0000	
AMETERS	0.0000	. 450	0.0000 38.1000	38.1000		38.1000	. 560	500	6000	.160	. 160	0.160	304 - 8000 0 - 0000 35 - 5600	
SOLID PAR	-292.1000	.100	0009.609-	-609.6000	000	-609.6000	000.0	.900	.500	3.571	0.000	000	203.2000	
	9.550 4.450 8.100	69.550	15.900 38.100	15.900 15.900	8.100	15.900	25.400	9.550	0.000	1.430	12.700	11.430 22.250	2000	4.450
	5.400	400	5.400	400	0.000	400	0.000	.400	1.600	.000	0.000	. 737	-101.6000 -25.4000 0.0000	. 700
SOLID NUM TYPE	31 TGC	32 ELLG	33 TGC	34 SPH		36 SPH 37 TGC)	38 ELLG	39 RPP 40 ELLG	1 ELL	2 ELL	43 ELLG	44 RPP 45 TGC	

TABLE C+I. GEOMETRIC SOLIDS COMPRISING COMPUTER MODEL OF STANDING CREW PERSONNEL (CONTINUED)

SOLI	LID			SOLID PAR	AMETERS			REMARKS
46	ELLG	25.400	5	0.900	50	000.0	. 41	G
		5.877	.000	8.001	000.	2.700	000.	¥ ⊇ ¥
47	R P	01.600	000.	.600	. 500	006.0	.200	HP THUM
48	ш	.937	2.250	52.500	.000	.400	.280	HT F
		000	1,430	.571	.160	.000	.000	FINGER
64	ELLG	.287	2.250	.500	.000	.000	.980	T SE
		0.000	2.700	.000	.160	.000	.000	FINGER
50	ELLG	.512	2.250	.500	.000	.000	.360	TH T
		000.	1.430	•000	.160	.000	.000	FINGER
51	ELLG	. 737	.250	-952.5000	000000	0.0000	-63.5000	RGT FOURTH
		000-	0.160	.000	0.160	.000	.000	INGE
52	<u>م</u>	1.600	5.400	4.800	3.200	.500	08.000	H DH
		.400	0.00	39.775	.000	000.	.200	DOME
		• 000	2.400	000	9.850	000	.000	
54	ELLG	.190	0.000	.775	.075	.000	.000	PELVIS
		00000	8.275	0	.000	000.	23.825	
55	160	.100	4.137	75	.350	000	.900	出
		00000	4.137	.000	19	.000	.000	THIGH
		.150	7.150					
56	160	8.100	.137	-739.7750	50	.000	-469.9000	RIGHT
		000.	4.137	000000	81.2673	0	0.0000	THIGH
		7.150	7.150					
57	TRC	4.450	4.137	-1209.6750	000000	0.000	-406.4000	iL.
		7.150	100					ш
58	TRC	4.450	4.137	-1209.6750	000000	0.0000	-406.4000	RIGHT
		7.150	8.100					ũ
59	ပ္သ	4.450	37	-1616.0750	000000	0.0000	-76.2000	u.
		8.100						ANK
9	RCC	28 1000	-84.1375	-1616.0750	00000	0.000	-76.2000	Ħ;
		7					•	ANNE

GEOMETRIC SOLIDS COMPRISING COMPUTER MODEL TABLE C-I.

	REMARKS	FOOT	R IGHT FOOT
		692.2750 692.2750 679.5750 616.0750	0000
CREW PERSONNEL (CONTINUED		134.9375 46.0375 134.9375 46.0375	6.037 4.937 6.037 4.937
I PERSONNEL	PARAMETERS	122.1740 -38.1000 122.1740 -38.1000	.10 .17 .10
STANDING CREV	SOLID PARA	-1692.2750 -1662.2750 -1666.8750 -1631.2515	69 69 69 63
OF S		46.0375 122.2375 46.0375 122.2375	6.037 6.037 2.237 2.237
		139.7000 -38.1000 139.7000 -38.1000	139.7000 -38.1000 139.7000 -38.1000
	SOLID NUM TYPE		OC AKBO

TABLE C-II. REGION COMBINATION TABLE FOR MODEL OF STANDING CREW PERSONNEL

REMARKS	HEAD TOP HEAD MIDDLE 19 HEAD LOWER NECK NOSE UPPER NOSE LOWER	CHIN BRAIN LEFT EYE RIGHT EYE	LEFT EAR -DUM LT EAR RIGHT EAR -DUM LT EYE -DUM LT EYE	-DUM RT EYE -DUM MOUTH -DUM HOTOP HELM UPRSEC -IN HELM SI HELM LWRSEC -IN HELM SI	-DUR HELMS2 SHOULDERS -DUM SHOULD THORAX LEFT ARM LT SHOULDJT RIGHT ARM
	- 18				
	-17				19 19 19
N DATA	-17	e e	- 23		-32
REGION COMBINATION	-16	-17	-21		-31 -31
EGION CO	-11 -10 -26 -7	-16	-15	-25	-30 -34 -36
α	110	-11	n m I I	75 7	1 1 1 1 1 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4
	••••••••••••••••••••••••••••••••••••••	-10		-21	27 -27 -30 -32
	11011411011	11000		2 0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	3 3 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
REGION NUMBER	ことのちょうらて	10 11 12	1 H H H H H	6 9 5 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	3 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5

TABLE C-II. REGION COMBINATION TABLE FOR MODEL OF STANDING CREW PERSONNEL (CONTINUED)

REMARKS	RT SHOULDJT	FT FOREAR	T ELBOW J	10		EF1	EFI	SE	-	-	···	—	SE	RIGHT PALM	191	SE	- -	<u></u>	···	, _	HS	800		EF	19 I	LEFT LEG	IGHT L	EFT ANKL	IGHT A	EFT FOOT	IGHT F
																													•		•
COMBINATION DATA																															
REGION COMB.							-40								-48								-56								
· &							-39								-47								-55								
		-34		-36			-37		77-	55-	55-	55-			-45		S	-52	5	5			S	S	S	-59	Ō	•	9		
	35																													61	
REGION NUMBER	32	ဗ	34	35	36	37	38	39	40	41	45	43	5 5	45	46	47	8 7	64	20	51	52	53	54	55	56	25	58	59	9	61	62

a section We to account to the test of the

TABLE C-III. REGION IDENTIFICATION TABLE FOR MODEL

	LOS Percent	100	100	100	100	25	25	25	100	100	100	100	100		100						100		100				100		100	100	000	
	MATERIAL CODE	81													83						7.7		77				87				& & &	
OF STANDING CREW PERSONNEL	DESCRIPTION	F HEAD - SKULL	IDDLE OF HEAD	OTTOM OF HEAD - SKUL	ECK	00	OSE - LOWE	OSTRIL	30	RAIN	EFT	IGHT	EFT	-DUMMY LEFT EAR	וצ	RIGHT EAR	LEFT	RIGHT EYE SOCK	-DUMMY MOUTH	HEAD TOP	JPPER SECTION	HELMET (OWER SECT		HELMET (SHAPES SECTION I	DUMMY HELMET (SHAPES SECTION 2	JL DERS	Ξ	XYX	ARM	LEFT SHOULDER JOINT RIGHT ARM	
	SPACE																															
	ITEM CODE	. ⊢	I	~	~	m	m	m	4	50	9	9	~	111		-	4	H	111	m	æ	111	80	111	Н	H	ው	111			11	
	REGION NUMBER	~	7	ന	4	'n	9	7	œ	O'	10	11	12	13	14	15	16	17	18	19	20	21	22	23	54	25	56	2.7	28	53	30 31	

TABLE C-III. REGION IDENTIFICATION TABLE FOR MODEL OF STANDING CREW PERSONNEL (CONTINUED)

LOS PERCENT	100	9 6	100		001	100) 	100	100	100	100		100	100		100	100	100	100		100	100	100	100	100	100	100	100	100	001
MATERIAL CODE	6- 0								68					89				68											8.6	
DESCRIPTION	RIGHT SHOULDER JOINT	בייוסאריין דייו	IGHT FORFARM	TOUT CLOSE	EFT PALM	EFT THUM	-DUMMY (SHAPE	EFT FIRST FINGE	SECO	EFT THIRD FINGE	EFT FOURTH FINGE	DUMMY (SHAPES	IGHT PALM	GHT THU	DUMMY (SHAPES R	IGHT FIRST FIN	IGHT SECOND FING	GHT THIRD FINGE	IGHT FOURTH FIN	DUMMY (SHAPES RI	80	ELVI	EFT THI	H	EFT L	IGHT LE	EFT ANKL	IGHT A	T F00	KIGH FUUS
SPACE CODE																														
ITEM	6 [-					H			H													14	
REGION NUMBER	8 6 2 6	7 7	+ IG (1)	76	0 E	80	36	40	41	42	43	77	45	46	47	84	64	50	51	52	53	54	55	56	57	58	59	9	61	70

REGION IDENTIFICATION TABLE FOR MODEL OF STANDING TABLE C-IV.

	LOS PERCENT	100	100	100	100	25	25	25	100	100	100	100	100	100	100	100	100	100	100	100	100	100	10c	100	100.	100	100	100	100	100	100	100
	MATERIAL Code	81	81	81	82	83	83	83	84	85	86	98	83	83	7.7	77	87	83	83	88	68	83	83	68	89	83	83	89	89	68	83	د 8
CREW PERSONNEL ORDERED BY ITEM NUMBER	DESCRIPTION	OP OF HEAD - SKUL	IDDLE OF HEAD - SK	OTTOM OF HEAD - SKUL	ZECK	NOSE - UPPER	OSE - LOWE	NOSTRILS	LOWER JAW - CHIN	BRAIN	EFT E	-	EFT E	IGHT EAR	ELMET U	ELMET LOWER SECTI	HOULDERS	EFT SHOULDER JOINT	IGHT SHOULDER JOI	HURAX	EFT ARM	IGHT ARM	EFT FOREARM	EFT ELB	IGHT FOREAR	RIGHT ELBOW JOINT	EFT PAL	EFT THUMB	EFT FIRST FING	2	EFT THIRD FINGER	EFT FOURTH FI
	SPACE																															
	ITEM		H	-	7	m	m	m	4	ī	9	9	7	~	80	80	Φ	6												11		
	REGION NUMBER		7	ന	4	2	9	7	80	Φ																				41		

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